IN THE SPECIFICATION:

Insert as the very first paragraph the following:

This application is a continuation of application Serial No. 09/953,954 filled September 18, 2001, which in turn is a continuation of application Serial No. 09/318,265 filed May 25, 1999, now Patent No. 6,352,756.

Change page 1, lines 8-16, to read:

The present invention relates to a honeycomb structure to be suitably used for use as a catalyst carrier for purifying automobile exhaust gas. More particularly, the present invention relates to a thin-walled honeycomb structure that has thin partition walls, a light weight, a small loss of pressure, and an improved mechanical strength. All improvements result by virtue of reinforcing a circumferential portion of the honeycomb structure, thereby preventing damage not so as to give the damages to the honeycomb structure during its manufacturing or its handling. The invention relates to a method for reinforcing such a thin-walled honeycomb structure.

Change page 2, line 2, to page 8, line 23, to read:

More concretely, a honeycomb structure has usually been produced by the steps of extrusion-molding a material, which mainly becomes cordierite when it is fired, through a nozzle having lattice-like slits so as to form integratedly a honeycomb portion and a circumferential wall, and subsequently drying and firing the thus molded article. The obtained honeycomb structure is transferred to a step of forming the catalytic layer by first firstly coating the inner surfaces of numerous cell passages with γ-alumina so as to form a γ-alumina layer thereon, and then loading a noble metal component, as a catalytic component, such as platinum, rhodium, or palladium into inner surfaces of pores of thus formed γ -alumina layer. Then, the honeycomb structure is subjected to a baking treatment at a temperature of about 600°C so as to back the catalytic component thereon to give a catalyst for purifying exhaust gas. Thus produced The resulting catalyst for purifying exhaust gas is housed in a metallic container with the

aid of a cushioning material. The metallic container, i.e., a converter is connected to an exhaust pipe by means of welding, bolting, or the like, to set up an engine for an automobile, etc.

Regulations Recently, regulations on exhaust gases have become stricter strict year by year, especially in developed countries, due to in consideration of environmental problems. To cope with these stricter regulations, an ever-lasting improvement purification ability is required for a catalyst for purifying exhaust gas. On the other hand, a desire to lower fuel charge and increase output of power has been evident in the fields of engine development. Because of such a situation, the reduction in pressure loss during operation has been required in the case of the catalyst for purifying exhaust gas. In the case of the catalyst for purifying exhaust gas, so as to solve the problems mentioned above, there have has become evident such a strong movement that the improvement in the performance of the catalyst for purifying exhaust gas at the time of warming warning up of the engine has been tried by increasing a passage area of the cell passages so as to reduce pressure loss. Furthermore, and lightening the weight of

the catalyst for purifying exhaust gas itself has been undertaken so as to reduce its heat capacity by making the partition walls thin without decreasing the number of cells as well. Hitherto, a honeycomb structure having partition walls of 0.15 mm or more in the thickness thick was most popular. However, a honeycomb structure having partition walls having a thickness of 0.13 or less, particularly, 0.11 mm or less, in the thickness has recently come to be popular.

However, to make partition walls of a honeycomb structure thinner causes a problem that the extremities (hereinafter sometimes referred to as a corner) of circumferential portions of the honeycomb structure are often broken during manufacturing, handling, or conveying the honeycomb structure, or housing the honeycomb structure into the container for converter so as to set it in an engine because the structural strength of the honeycomb structure is consequently decreased, particularly in the circumferential portions of the honey-comb structure. This phenomenon becomes evident when the partition walls of the honeycomb structure becomes become thinner. This is because damage

occurs damages have recently come to be caused in a honeycomb structure more frequently when in accordance with thinning of partition walls in a honeycomb structure are thinned. Note that the honeycomb structure is liable to break when an external force such as a mechanical shock is applied thereto during transportation or the like, even in the case of the honeycomb structure having thicker partition walls. This is potential breakage occurs because a ceramic material is inherently brittle. Thus, the breaking of the honeycomb structure was also occasionally reported. Because of its very low frequency of occurrence, however, it has not particularly been regarded as a problem.

Further, the frequency of the deformation in partition walls during extrusion-molding has remarkably increased as partition walls become thinner; while in the case of the conventional honeycomb structures having such thicker partition walls as the thickness of that are 0.15 mm or more thick, such a problem is not so serious. This is because the circumferential wall has a thickness of at least 0.3 mm, and therefore, the strength in the circumferential portion can be ensured to a certain degree. The

deformation in partition walls because mainly tends to be caused particularly at the vicinity of the circumferential walls in the circumferential portions. This deformation is due to Its major cause is considered to be the failure to attain uniform extrusion-molding because of the unbalance in the fluidity of a raw material between the honeycomb portions and the vicinity of the circumferential partition walls, in the case where when the circumferential walls are made thicker than partition walls. Such thickening ensures in a honeycomb structure so as to ensure strength in the circumferential portion.

A similar phenomenon when using to the case where cordierite to deform is used in the deformation of the partition walls in the honeycomb structure is also observed when a ceramic material such as alumina, mullite, silicon nitride, silicon carbide, or zirconia is subjected to an extrusion-molding. This phenomenon occurs is because, as a starting material, a material prepared by mixing and kneading said the starting material with water and a binder is used as well. Since the deformation in partition walls is mainly attributed to buckling derived from compressive load, a similar

problem is also observed in not only a honeycomb structure having square cells, but also <u>in</u> a honeycomb structure having <u>s</u> rectangular, triangular, or hexagonal shape.

Some proposals have been made to solve the various problems derived caused by making partition walls thinner in a honeycomb structure. First Firstly, it has been proposed to reduce make the thickness of the circumferential walls from 0.3 mm to 0.1 mm. Thus, so as to near the thickness of the circumferential walls approximates the to a thickness of the partition walls, thereby improving in order to improve the balance in the flow amount of a raw material during molding. In this case, however, the strength of in the circumferential wall is not sufficient. In other words, when circumferential walls are too thin, a breaking starts at the circumferential walls due to its insufficient rigidity. circumferential wall was thickness of at least 0.1 mm, desirably at least 0.15 mm, is sufficient just to house the honeycomb structure in into a container kept under a uniform and static external pressure as a thickness for carcumferential walls. However, such a chroumferential well thickness for the circumferential walls is not

mechanical shock given during transport transporting the honeycomb structure or the like.

On the other hand, there has been made such a proposal it has been proposed that the strength against mounting pressure of the circumferential walls would increase if the thickness of the circumferential walls are thickened is made thicker. Thus, a cordierite honeycomb structure having square cells, a partition wall thickness of 0.11 mm, and a circumferential wall such a thickness of at least 0.4 mm as circumferential walls was prepared increase strength. Contrary On the contrary expectation, however, it was found, as a result of an isostatic strength test, that the honeycomb structure was not improved in strength and had a tendency of deterioration in strength. The Aninvestigation was made so as to clarify the reason why the isostatic strength could not improve when only the thickness of the circumferential walls was made thicker. As a result, it has been found that partition walls (ribs) around cells in the circumference in a molded article are deformed to a great extent just after

extrusion- molding, and that the number of deformed partition walls increases as the circumferential wall is made thicker.

If This is because, if the circumferential wall is thickened, the made thicker, an amount of a raw material passing through slits for forming the circumferential walls increases when the raw material passes through slits of the nozzle upon extrusion-molding. As a consequence, partition walls around circumferential cells are dragged pulled toward the circumferential walls, or circumferential walls press the internal partition walls of the honeycomb structure. Thus, it has been evident that the remarkable gap in the unbalance between a flow of the raw material for the circumference wall and a flow of the raw material for the partition walls is considered to be a major cause. Further, the thinning of the partition walls brings buckling deformation more easily. addition, the circumferential wall and partition walls in the circumferential portion are deformed by the weight of the honeycomb structure itself at the time when a honeycomb structure is supported by a jig on the surface of the circumferential walls

right after extrusion-molding. These are also considered to be the $\frac{major}{main}$ main causes.

If the internal partition walls of the honeycomb structure 48 are molded straight, the breakage of the honeycomb structure starts owing to the compression of the partition walls when pressure is given applied to the honeycomb structure from the surface side of the circumferential wall. This is because the internal portion of the honeycomb structure is theoretically the center of compressive stress. However, in the case where that partition walls at the vicinity of the circumferential portion are is deformed, or when that the circumferential wall is extremely thin, bending stress, i.e., a tensile stress is generated at the position of partition walls of the honeycomb structure. Since the a ratio of tensile strength to compressive strength is generally as low as about 1:10, the honeycomb structure starts to break if it has deformed partition walls when even only very low strength is given thereto.

On the other hand, even if the circumferential wall can be made considerably thickened thickened the time of molding, a great

difference in heat capacity exists between the honeycomb portion having thin partition walls and the thick circumferential wall, thereby Lowering the thermal shock resistance of the honeycomb heater is lowering the thermal shock resistance of the honeycomb

In order to solve the problems derived from an extreme difference in thickness between the honeycomb portion and the circumferential portion, there has been made the following proposal has been made; a molding is carried out, with the adjustment of a raw material flow at the time of extrusion, by making partition walls in the circumferential portion and the circumferential wall thicker so as to enhance pressure resistance in an axial direction of the honeycomb structure and a molding is carried out by adjusting. However, since the adjustment of balance is very subtle when this means is used, it becomes more difficult to suppress deformation in the partition walls as the circumferential wall becomes thicker. Furthermore, the thicker circumferential portion gaves has a greater influence on its own heat capacity. In this case, the temperature difference in temperature between the inside and the outside of the circumferential wall increases; is increased;

thereby thermal shock resistance of the honeycomb structure and inevitably decreases eccreased. Furthermore, since such means brings about an increase in weight of the honeycomb structure, the performance of the catalyst after of an engine is warmed up is lowered. Furthermore, it is not so preferable due to the pressure loss problem.

Change page 10, lines 7-22, to read:

The present invention has been made, taking into consideration the aforementioned conventional problems. Thus, the aim of the present invention is to provide a honeycomb structure having not only sufficient catalytic properties, mechanical strength, and thermal shock resistance, but also having a reinforced circumferential portion that is not so as to be damaged during manufacturing or handling the honeycomb structure. According to the present invention, there is provided a thin-walled honeycomb structure comprising:

a circumferential wall,

numerous partition walls disposed inside the circumferential wall cage postions, defined by the partition walls meeting the circumferential wall, and

numerous cell passages defined by the partition walls and a coat of reinforcing material covering the circumferential wall;

wherein a circumferential portion of the honeycomb structure is reinforced wholly or in a part within a certain distance from an extremity surface of the honeycomb structure by a reinforcing material which that dissipates, or evaporate evaporates at a high temperature, thereby protecting the edge portions of the honeycomb structure from damage before the structure is fired.

Change page 11, lines 8-18, to read:

According to the present invention, there is further provided a method for reinforcing a thin-walled honeycomb structure comprising:

presenting a honeycomb structure having a circumferential wall,

numerous partition walls disposed inside the circumferential wall, and

numerous cell passages defined by the partition walls;

wherein a circumferential portion of the honeycomb structure is coated wholly or in a part within a certain distance from an extremity surface of the honeycomb structure with an organic high molecular weight material.

Change page 12, line 22, to page 13, line 11, to read:

Fig. 1 is a perspective view showing an unreinforced embodiment of a thin-walled honeycomb structure; of the present anyention

Fig. 2 is a view of the presently claimed invention according to examples 1-4;

Fig. 3 is a view of the presently claimed invention according to examples 5 and 6, and

Fig. 4 is a view of the presently claimed invention according to examples 7-1.4.

Detailed Description of Mode for Carrying Out the Invention

A thin-walled honeycomb structure of the present invention has the same structure and basic shape as a conventionally known general honeycomb structure 1. As shown in a perspective view of Fig. 1, the thin-walled honeycomb structure is constituted by a circumferential wall 2, numerous partition walls 3 disposed inside the circumferential wall 2, and numerous cell passages 4 (cells 4) defined by the partition walls 3. Though each of the cells 4 has a square shape (sectional shape) in Fig. 1, it may also be triangular, rectangular, hexagonal, circular, or the like.

Page 19, line 4, cancel the title Example and replace with:

Examples

Change page 21, line 11 to page 23, line 1, to read:

Fig. 2 illustrates In each of the Examples 1 and 2, in which the surface of the circumferential wall 2 was impregnated with a resin 6. A mixture liquid having an adequately low viscosity was prepared by mixing a polyamide curing agent, a solvent, and a plasticizer with a commercially available epoxy resin. A honeycomb structure in which the entire surface of the end was masked with a tape was immersed in the liquid by about approximately 10 mm from its extremity and surfaces, leaving a band of uncoated surface 5, so that the circumferential wall of the honeycomb structure was impregnated with liquid. After the surface of the the circumferential wall was coated with the resin liquid to a certain degree, the honeycomb structure was taken out, and the resin liquid sticking to the circumferential wall was wiped off. The honeycomb structure was put in a drying container so as to be subjected to a thermal curing treatment at about 150°C for 30 minutes, thereby reinforcad honeycomb structure 20. producing resin ವ

In Examples 3 and 4, both shows in Fig. 2, a resin 6 was applied on the circumferential wall 2. An adhesive which that had been prepared by mixing a nitrile rubber with a commercially

available thermosetting phenol resin was applied on the circumferential wall, thereby forming an adhesive layer having a thickness of 1 - 2 mm and a width of approximately 10 mm from the end surfaces of the honeycomb structure was formed over the whole circumference of the circumferential wall in a narrow band. Then the honeycomb structure was subjected to heat-curing treatment at about 180°C for 30 minutes, thereby producing a resin reinforced honeycomb structure 20.

Fig. 3 illustrates the Examples 5 and 6, in which a resin was filled into cells in the circumferential portion. First, a mixture liquid having an adequately low viscosity was prepared by adding a polyamide curing agent, a solvent, and a plasticizer to an epoxy resin. A honeycomb heaten structure whose end surfaces were extremity was masked with a tape so as to exclude cells in the most circumferential portion was immersed in the liquid by about to a depth of approximately 10 mm. After the liquid was filled into the circumferential cells 7, the honeycomb structure was taken out. The liquid sticking to the surface of the circumferential wall was wiped off. Then, the honeycomb structure was put in a drying

container and subjected to a heat-curing treatment for about 150°C for 30 minutes, thereby producing a mesin circumferential cell and surface meanflowed honeycomb structure 30.

Fig. 4 fillustrates In Examples 7 - 14, in which a tape 8 was put on the surface of the circumferential wall 2. A rubber pressure-sensitive adhesive was applied on one side of a thin sheet. An adhesive tape having a thickness of 1 - 2mm was cut so as to have a width of approximately 10mm. The tape 8 was wound around the circumferential wall by with being pressed against the surface of the wall to cover the range within approximately 10mm from the end of the honeycomb structure, thus leaving an uncoated surface 5. This treatment results in a tape meinforced honeycomb structure 40

Page 23, after line 16, insert the following:

The Sollowing is a summary of the reinforcement of the circumferential portions in Sable :

Comparative Example 1.

The cell passages on the circumferential portion and the circumferential wall were filled with a ceramic until the depth of approximately 10 mm from the end surface. The resultant was refired.

Comparative Example 2:

A ceramic was immersed at the circumferential wall of the structure up to the distance of approximately 10 mm from the end surface. The resultant was refired.

Comparative Examples 3 to 6:

No reinforcement

Comparative Examples 7 and 8:

A ceramic was immersed at the circumferential wall of the structure up to the distance of approximately 10 mm from the end surface. The resultant was refired.

Examples 1 and 2:

A mesin was immersed at the circumferential wall of the structure up to the distance of approximately 10 mm from the end surface. The resultant was subjected to curing of the resin.

Examples 3 and 6:

A resin was coated at the circumferential wall of the structure up to the distance of approximately 10 mm from the end surface. The resultant was subjected to curing of the resin.

Examples 5 and 6:

The cell passages on the circumferential portion of the structure were filled with a resin to a height approximately 10 mm from the end surface. The resultant was subjected to curing of the resin.

Examples 7 and 14:

An adhesive tape was adhered on the circumferential wall of the structure, the tape width being approximately 10 mm from the end surface.